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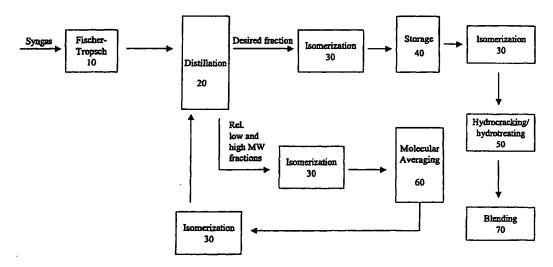
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(54) Title: SYNTHESIS OF NARROW LUBE CUTS FROM FISCHER-TROPSCH PRODUCTS



(57) Abstract: A process for preparing hydrocarbons in the lube base oil range, lube base oils and lube oil compositions from a fraction with an average molecular weight above a target molecular weight and a fraction with an average molecular weight below a target molecular weight via molecular averaging is described. The fractions can be obtained, for example, from Fischer-Tropsch reactions, and/or obtained from the distillation of crude oil. Molecular averaging converts the fractions to a product with a desired molecular weight, for use in preparing a lube oil composition. The product can optionally be isomerized to lower the pour point, and also can be blended with suitable additives for use as a lube oil composition.

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1	SYNTHESIS OF NARROW LUBE CUTS
2	FROM FISCHER-TROPSCH PRODUCTS
3	
4	RELATED APPLICATION
5	
6	This application is related to "Process for Conversion of Natural Gas and
7	Associated Light Hydrocarbons to Salable Products" by Dennis J. O'Rear,
8	Charles L. Kibby and Russell R. Krug, filed concurrently with this application.
9	
10	FIELD OF THE INVENTION
11	
12	This invention relates to the molecular averaging of various feedstocks to form
13	lube oils.
14	
15	BACKGROUND OF THE INVENTION
16	
17	There is a need for lubricating oils in the C ₃₀ + range which have a high
18	viscosity index (VI) and good oxidation stability. The majority of lubricating
19	oils used in the world today are derived from crude oil, and include a
20	petroleum base oil and an additive package. The base oils are refined from
21	crude oil through a plurality of processes such as distillation, hydrocracking,
22	hydroprocessing, catalytic dewaxing, and the like. Hydrocarbons in the lube
23	oil boiling range from these processes needs to be further processed to create
24	the finished base oil. In creating the base oil, the refiner desires to obtain the
25	highest possible yield while preserving the VI of the oil.
26	
27	Crude oil fractions in the C_{30} + range often tend to include waxes. Since the
28	presence of wax in lube oil adversely affects various physical properties, such
29	as the pore point and cloud point, the waxy components are typically
30	removed. The waxy components of the oil can be removed using various
31	processes, including solvent dewaxing and/or catalytic dewaxing, both of

which tend to provide lower yields at a given VI. It would be highly desirable 1 to have a process that optimizes the yield of lube oil at a given VI. 2 3 The use of crude oil as a feedstock for preparing lube oils is limited by the 4 product loss associated with the steps required to remove the waxy 5 components. Further, crude oil is in limited supply, it includes aromatic 6 compounds believed to cause cancer, and contains sulfur and nitrogen-7 containing compounds that can adversely affect the environment. 8 9 Lube oils can also be prepared from natural gas. This involves converting 10 natural gas, which is mostly methane, to synthesis gas (syngas), which is a 11 mixture of carbon monoxide and hydrogen, and subjecting the syngas to 12 Fischer-Tropsch reaction conditions. An advantage of using fuels prepared 13 from syngas is that they do not contain significant amounts of nitrogen or 14 sulfur and generally do not contain aromatic compounds. Accordingly, they 15 have minimal health and environmental impact. 16 17 A limitation associated with Fischer-Tropsch chemistry is that it tends to 18 produce a broad spectrum of products, ranging from methane to wax. While 19 the product stream includes a fraction useful as lube oils, it is not the major 20 product. Product slates for syngas conversion over Fischer-Tropsch catalysts 21 (for example, Fe, Co and Ru) are controlled by polymerization kinetics with 22 fairly constant chain growth probabilities that fix the possible product 23 distributions. Heavy products with a relatively high selectivity for wax are 24 produced when chain growth probabilities are high. Methane is produced with 25 high selectivity when chain growth probabilities are low. 26 27 It is generally possible to isolate various fractions from a Fischer-Tropsch 28 reaction, for example, by distillation. The fractions include, among others, a 29 gasoline fraction (B.P. about 68-450°F/20-232°C), a middle distillate fraction 30 (B.P. about 250-750°F/121-399°C), a wax fraction (B.P. about 31

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650-1200°F/343-649°C) primarily containing C20 to C50 normal paraffins with a 1 small amount of branched paraffins and a heavy fraction (B.P. above about 2 1200°F/649°C) and tail gases. A suitable fraction for use in preparing a lube 3 oil can be isolated from the product stream by distillation. However, 4 depending on market considerations, it might be advantageous to provide a 5 process that would convert the other fractions into fractions suitable for use in 6 preparing lube oils. The present invention provides such a process. 7 8 SUMMARY OF THE INVENTION 9 10 In its broadest aspect, the present invention is directed to an integrated 11 process for producing hydrocarbons in the lube base oil range, lube base oils 12 and lube oils. As used herein, lube base oils are generally combined with an 13 additive package to provide finished lube oils. Hydrocarbons in the lube base 14 oil range are prepared via molecular averaging of a relatively low molecular 15 weight fraction and a relatively high molecular weight fraction. 16 17 The resulting hydrocarbons tend to be waxy unless they are isomerized prior 18 to the molecular averaging step. Isomerization of the hydrocarbons provides 19 a lube base oil, which, when combined with the additive package, provides a 20 lube oil composition. Catalytic isomerization improves the pour point and 21 viscosity index. Hydrotreatment can optionally be performed on the 22 hydrocarbons or lube base oil to hydrotreatment to remove olefins, 23 24 oxygenates and other impurities. 25 Depending on the desired physical and chemical properties of the lube oil 26 composition, the product of the molecular averaging reaction can include 27 virtually any combination of hydrocarbons between C₂₀ and C₅₀. Preferably, 28 the lube oil composition includes mostly hydrocarbons in the range of around 29 C₃₀. When preparing a lube base oil composition in the C₂₀ to C₅₀ range, one 30 can combine hydrocarbon materials below C₂₀ and above C₅₀ and subject 31

1	them to molecular averaging to arrive at a composition in the desired range.
2	When preparing a lube base oil composition in the C_{30} range, for example, C_{20}
3	and C ₄₀ fractions can be combined and subjected to molecular averaging.
4	
5	In one embodiment, the process involves performing Fischer-Tropsch
6	synthesis on syngas to provide a range of products, isolating various fractions
7	via fractional distillation, and performing molecular averaging on a relatively
8	low molecular weight fraction and a relatively high molecular weight fraction to
9	provide a product with a molecular weight between the low and high
0	molecular weights, which is suitable for use in preparing a lube base oil
1	composition. In another embodiment, relatively low molecular weight and/or
2	relatively high molecular weight fractions are obtained from another source,
3	for example, via distillation of crude oil, provided that the fractions do not
4	include appreciable amounts (i.e., amounts which would adversely affect the
5	catalyst used for molecular averaging) of thiols, amines, or cycloparaffins.
6	
7	It may be advantageous to take representative samples of each fraction and
8	subject them to molecular averaging reactions, adjusting the relative
9	proportions of the fractions until a product with desired properties is obtained.
20	Then, the reaction can be scaled up using the relative ratios of each of the
21	fractions that resulted in the desired product. Using this method, one can "dial
22	in" a molecular weight distribution which can be roughly standardized between
23	batches and result in a reasonably consistent product.
24	
25	BRIEF DESCRIPTION OF THE DRAWING
26	
27	The Figure is a schematic flow diagram representing one embodiment of the
28	invention.
20	

DETAILED DESCRIPTION OF THE INVENTION

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In its broadest aspect, the present invention is directed to an integrated process for producing hydrocarbons in the lube base oil range, lube base oils and lube oils via molecular averaging of relatively low molecular weight and relatively high molecular weight fractions, for example, C_{20} and C_{40} fractions. The lube base oil composition includes hydrocarbons in the range of between about C_{20} and C_{50} , but is preferably around C_{30} .

8

10 As used herein, "hydrocarbons in the lube base oil range" are hydrocarbons 11 having a boiling point in the lube oil range (i.e., between 650°F and 1200°F). 12 As used herein, a "relatively low molecular weight fraction" is a fraction with 13 an average molecular weight lower than the average molecular weight of the 14 desired lube oil composition. A "relatively high molecular weight fraction" is a 15 fraction with an average molecular weight higher than the average molecular 16 weight of the desired lube oil composition. "Average molecular weight" is 17 molar average molecular weight. Preferably, the relatively high and relatively 18 low molecular weight fractions are each within about 10 carbons from that of 19 the desired product. However, the process described herein can tolerate 20 broader differences in molecular weight.

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An important consideration for determining an appropriate ratio of high molecular weight and low molecular weight fractions is that the average molecular weight of the two fractions, taking into consideration the relative proportions of each fraction, is close to the desired average molecular weight. Because of reactivity differences, it is possible to have an excess of one component, in particular, the lower molecular weight fraction.

28 29

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In one embodiment, the process involves performing Fischer-Tropsch synthesis on syngas to provide a range of products, isolating various fractions via fractional distillation (including relatively high and relatively low molecular

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1	weight fractions), and performing molecular averaging on the relatively low
2	molecular weight and relatively high molecular weight fractions. Alternatively,
3	the relatively low molecular weight and/or relatively high molecular weight
4	fractions are obtained from another source, for example, via distillation of
5	crude oil, provided that the fractions do not include an appreciable amount of
6	olefins, heteroatoms or saturated cyclic compounds.
7	
8	The product from the molecular averaging reaction typically includes
9	hydrocarbons with molecular weights between the low and high molecular
10	weights. A suitable fraction can be isolated, for example, by distillation, which
11	fraction contains hydrocarbons in the lube base oil range. These
12	hydrocarbons generally are waxy solids, but can be readily isomerized to form
13	a lube base oil composition. The lube base oil composition can be blended
14	with suitable additives to form the lube base oil composition.
15	\cdot
16	The process described herein is an integrated process. As used herein, the
17	term "integrated process" refers to a process which involves a sequence of
18	steps, some of which may be parallel to other steps in the process, but which
19	are interrelated or somehow dependent upon either earlier or later steps in the
20	total process.
21	
22	An advantage of the present process is the effectiveness with which the
23	present process may be used to prepare high quality base oils useful for
24	manufacturing lubricating oils, and particularly with feedstocks which are not
25	conventionally recognized as suitable sources for such base oils.
26	
27	Lube Base Oil Composition
28	
29	The lube base oil prepared according to the process described herein can
30	have virtually any desired molecular weight, depending on the desired
31	physical and chemical properties of the lube oil composition, for example,
32	pour point, viscosity index and the like. The molecular weight can be

controlled by adjusting the molecular weight and proportions of the high 1 molecular weight and low molecular weight fractions. Lube oil compositions 2 with boiling points in the range of between about 650°F and 1200°F are 3 preferred, with boiling points in the range of between about 700°F and 1100°F 4 being more preferred. The currently most preferred average molecular weight 5 is around C₃₀, which has a boiling point in the range of roughly 840°F, 6 depending on the degree of branching. However, the process is adaptable to 7 generate higher molecular weight lube oils, for example, those in the C₃₅-C₄₀ 8 range, or lower molecular weight lube oils, for example, those in the C20-C25 9 range. Preferably, the majority of the composition includes compounds within 10 about 8 carbons of the average, more preferably, within around 5 carbons of 11 12 the average. 13 In a preferred embodiment, the composition includes branched hydrocarbons. 14 The products of the Fischer-Tropsch synthesis tend to be linear, which can 15 result in a relatively high pour point. However, the linear products can be 16 isomerized readily using known isomerization chemistry, or, alternatively, the 17 reactants subjected to molecular averaging can be isomerized before the 18 molecular averaging step. Accordingly, the preferred lube base oil 19 composition can generally be described as including hydrocarbons in the 20 C₂₀-C₅₀, preferably around C₃₀ range which include branching typical of that 21 22 observed in compositions subjected to catalytic dewaxing and/or 23 isomerization dewaxing processes. 24 The lube base oil and/or lube oil preferably have a pour point in the range of 25 10°C or lower, more preferably 0°C or lower, still more preferably, -15°C or 26 lower, and most preferably, between -15°C and -40°C. The degree of 27 branching in the composition is preferably kept to the minimum amount 28 needed to arrive at the desired pour point. Pour point depressants can be 29 30 added to adjust the pour point to a desired value. 31

- 1 The lube base oil and/or lube oil composition preferably have a kinematic
- 2 viscosity of at least 3 centistokes, more preferably at least 4 centistokes, still
- 3 more preferably at least 5 centistokes, and most preferably at least
- 4 6 centistokes, where the viscosity is measured at 40°C. They also have a
- 5 viscosity index (a measure of the resistance of viscosity change to changes in
- 6 temperature) of at least 100, preferably 140 or more, more preferably over
- 7 150, and most preferably over 160.

8

9 Another important property for the lube base oil and lube oil composition is

- 10 that it has a relatively high flash point for safety reasons. Preferably, the flash
- point is above 90°C, more preferably above 110°C, still more preferably
- greater than 175°C, and most preferably between 175°C and 300°C. The
- 13 following table (Table 1) shows a correlation between viscosity and flash point
- 14 of preferred lubricants for use in automobiles.

15

16

Table 1

Flash Point (D93), °C	Flash Point (D92), °C
175	175
205	208
201	214
230	237
251	269
	175 205 201 230

17 18

*D92 and D93 listed in the above table refer to ASTM tests for measuring flash point:

19 20

21 Flash Point, COC, °C

D 92

22 Flash Point, PMCC, °C

D 93

23

24 The lube oil can be used, for example, in automobiles. The high paraffinic

25 nature of the lube oil gives it high oxidation and thermal stability, and the lube

oil has a high boiling range for its viscosity, i.e., volatility is low, resulting in

27 low evaporative losses.

1	The lube oil can also be used as a blending component with other oils. For
2	example, the lube oil can be used as a blending component with
3	polyalphaolefins, or with mineral oils to improve the viscosity and viscosity
4	index properties of those oils, or can be combined with isomerized petroleum
5	wax. The lube oils can also be used as workover fluids, packer fluids, coring
6	fluids, completion fluids, and in other oil field and well-servicing applications.
7	For example, they can be used as spotting fluids to unstick a drill pipe that
8	has become stuck, or they can be used to replace part or all of the expensive
9	polyalphaolefin lubricating additives in downhole applications. Additionally,
10	they can also be used in drilling fluid formulations where shale-swelling
11	inhibition is important, such as those described in U.S. Pat. No. 4,941,981 to
12	Perricone et al.
13	
14	Preferably, the lube oil is obtained via molecular averaging of Fischer-Tropsch
15	products and, therefore, contains virtually no heteroatoms or saturated cyclic
16	compounds. Alternatively, the lube oil can be obtained by molecular
17	averaging of other feedstocks, preferably in which at least the heteroatoms,
18	and more preferably the saturated cyclic compounds, have been removed.
19	
20	Additives
21	
22	The lube oil composition includes various additives, such as lubricants,
23	emulsifiers, wetting agents, densifiers, fluid-loss additives, viscosity modifiers,
24	corrosion inhibitors, oxidation inhibitors, friction modifiers, demulsifiers,
25	anti-wear agents, dispersants, anti-foaming agents, pour point depressants,
26	detergents, rust inhibitors and the like. Other hydrocarbons, such as those
27	described in U.S. Patent No. 5,096,883 and/or U.S. Patent No. 5,189,012,
28	may be blended with the lube oil provided that the final blend has the
29	necessary pour point, kinematic viscosity, flash point, and toxicity properties.
30	The total amount of additives is preferably between 1-30 percent. All
31	percentages listed herein are weight percentages unless otherwise stated.
32	

1	Examples of suitable lubricants include polyol esters of C ₁₂ -C ₂₈ acids.
2	
3	Examples of viscosity modifying agents include polymers such as ethylene
4	alpha-olefin copolymers which generally have weight average molecular
5	weights of from about 10,000 to 1,000,000 as determined by gel permeation
6	chromatography.
7	
8	Examples of suitable corrosion inhibitors include phosphosulfurized
9	hydrocarbons and the products obtained by reacting a phosphosulfurized
10	hydrocarbon with an alkaline earth metal oxide or hydroxide.
11	
12	Examples of oxidation inhibitors include antioxidants such as alkaline earth
13	metal salts of alkylphenol thioesters having preferably C ₅ -C ₁₂ alkyl side chain
14	such as calcium nonylphenol sulfide, barium t-octylphenol sulfide,
15	dioctylphenylamine, as well as sulfurized or phosphosulfurized hydrocarbons.
16	Additional examples include oil soluble antioxidant copper compounds such
17	as copper salts of C ₁₀ to C ₁₈ oil soluble fatty acids.
18	
19	Examples of friction modifiers include fatty acid esters and amides, glycerol
20	esters of dimerized fatty acids and succinate esters or metal salts thereof.
21	
22	Dispersants are well known in the lubricating oil field and include high
23	molecular weight alkyl succinimides being the reaction products of oil soluble
24	polyisobutylene succinic anhydride with ethylene amines such as
25	tetraethylene pentamine and borated salts thereof.
26	
27	Pour point depressants such as C ₈ -C ₁₈ dialkyl fumarate vinyl acetate
28	copolymers, polymethacrylates and wax naphthalene are well known to those
29	of skill in the art.
30	
31	Examples of anti-foaming agents include polysiloxanes such as silicone oil
32	and polydimethyl siloxane; acrylate polymers are also suitable.

1 Examples of anti-wear agents include zinc dialkyldithiophosphate, zinc diaryl 2 3 diphosphate, and sulfurized isobutylene. 4 5 Examples of detergents and metal rust inhibitors include the metal salts of 6 sulfonic acids, alkylphenols, sulfurized alkylphenols, alkyl salicylates, 7 naphthenates and other oil soluble mono and dicarboxylic acids such as 8 tetrapropyl succinic anhydride. Neutral or highly basic metal salts such as 9 highly basic alkaline earth metal sulfonates (especially calcium and 10 magnesium salts) are frequently used as such detergents. Also useful is 11 nonylphenol sulfide. Similar materials made by reacting an alkylphenol with 12 commercial sulfur dichlorides. Suitable alkylphenol sulfides can also be 13 prepared by reacting alkylphenols with elemental sulfur. Also suitable as 14 detergents are neutral and basic salts of phenols, generally known as 15 phenates, wherein the phenol is generally an alkyl substituted phenolic group, 16 where the substituent is an aliphatic hydrocarbon group having about 4 to 400 17 carbon atoms. 18 19 Antioxidants can be added to the lube oil to neutralize or minimize oil 20 degradation chemistry. Examples of antioxidants include those described in 21 U.S. Pat. No. 5,200,101, which discloses certain amine/hindered phenol, acid 22 anhydride and thiol ester-derived products. 23 The combination of a metallic dithiophosphate hydroperoxide decomposer 24 25 and aminic antioxidant is reported to have a synergistic effect on lubricant antioxidant performance. See Maleville et al., Lubrication Science, V9, No. 1, 26 27 pg. 3-60 (1996). Sulfur-substituted derivatives of mercapto carboxylic esters 28 also are reported to possess antioxidant properties. See M. A. Mirozopeva 29 et al., Naftekhimiya, V28, No. 6, pg. 831-837 (1988). 30 31 Additional lube oils additives are described in U.S. Patent No. 5,898,023 to 32 Francisco et al., the contents of which are hereby incorporated by reference.

Feedstocks for the Molecular Averaging Reaction

Examples of feedstocks that can be molecularly averaged in accordance with the present invention include oils that generally have relatively high pour points which it is desired to reduce to relatively low pour points. Numerous petroleum feedstocks, for example, those derived from crude oil, are suitable for use. Examples include petroleum distillates having a normal boiling point above about 100°C, gas oils and vacuum gas oils, residuum fractions from an atmospheric pressure distillation process, solvent-deasphalted petroleum residues, shale oils, cycle oils, petroleum and slack wax, waxy petroleum feedstocks, NAO wax, and waxes produced in chemical plant processes. Straight chain n-paraffins either alone or with only slightly branched chain paraffins having 16 or more carbon atoms are sometimes referred to herein as waxes.

The feedstocks should not include appreciable amounts of olefins, heteroatoms, or saturated cyclic compounds. Preferred feedstocks are products from Fischer-Tropsch synthesis or waxes from petroleum products. If any heteroatoms, olefins or saturated cyclic compounds are present in the feedstock, they should be removed before the molecular averaging reaction. Olefins and heteroatoms can be removed by hydrotreating. Saturated cyclic hydrocarbons can be separated from the desired feedstock paraffins by use of adsorption with molecular sieves or by deoiling or by complexing with urea.

Preferred petroleum distillates for use in the relatively low molecular weight fraction boil in the normal boiling point range of 200°C to 700°C, more preferably in the range of 260°C to 650°C. Suitable feedstocks also include those heavy distillates normally defined as heavy straight-run gas oils and heavy cracked cycle oils, as well as conventional FCC feed and portions thereof. Cracked stocks may be obtained from thermal or catalytic cracking of various stocks. The feedstock may have been subjected to a hydrotreating

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